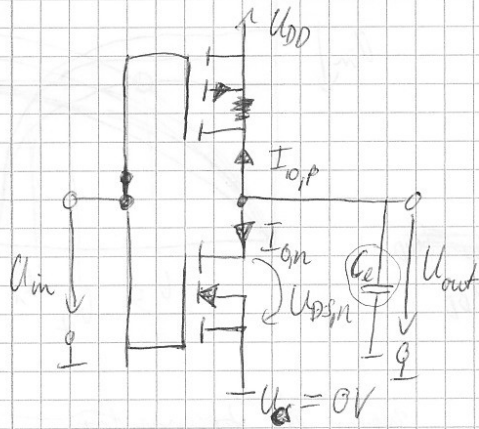
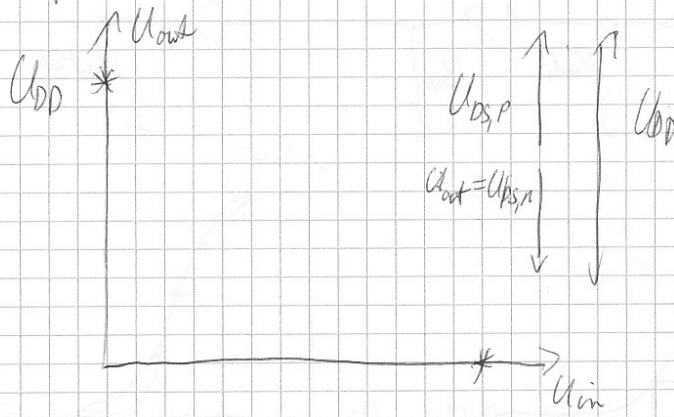
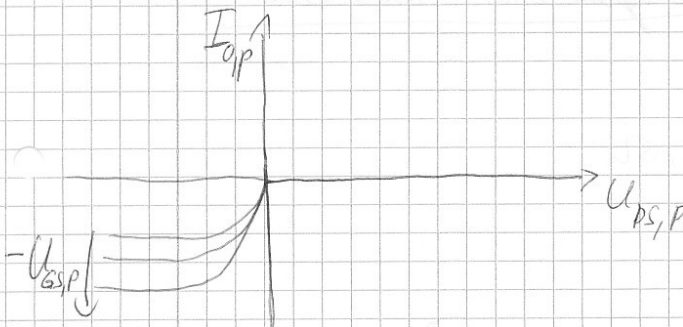
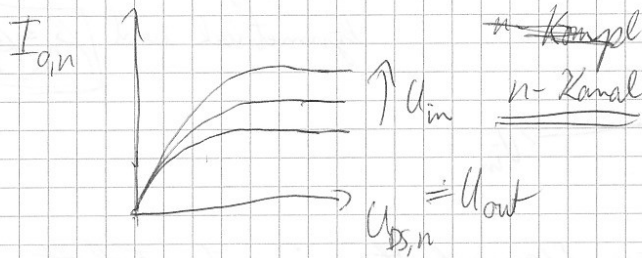
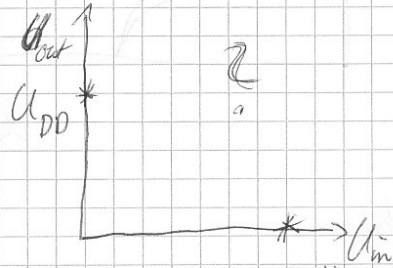


13) CMOS - Inverter Inverter



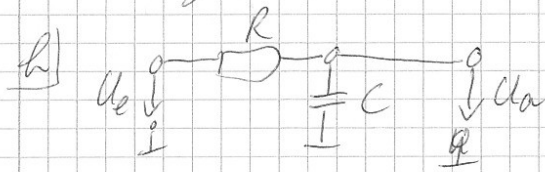
$\beta_n = \beta_p$

$U_{E,n} = -U_{E,p}$



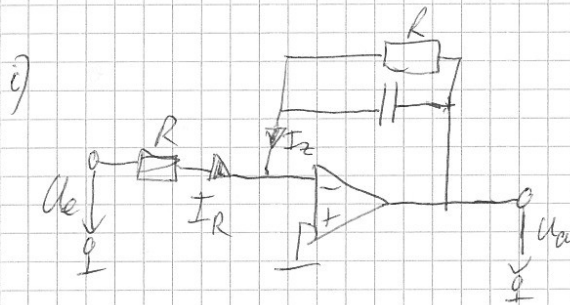
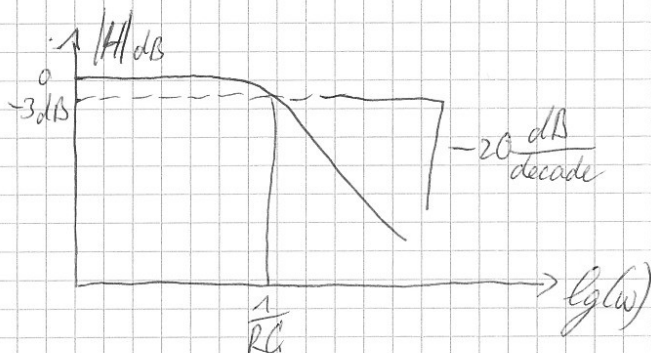
T13-Übung

29.7.07



$$U_a = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} \quad U_e = \frac{U_e}{1 + j\omega RC}$$

$$H(j\omega) = \frac{U_a}{U_e} = \frac{1}{1 + j\omega RC}$$



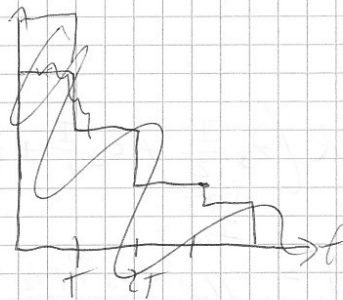
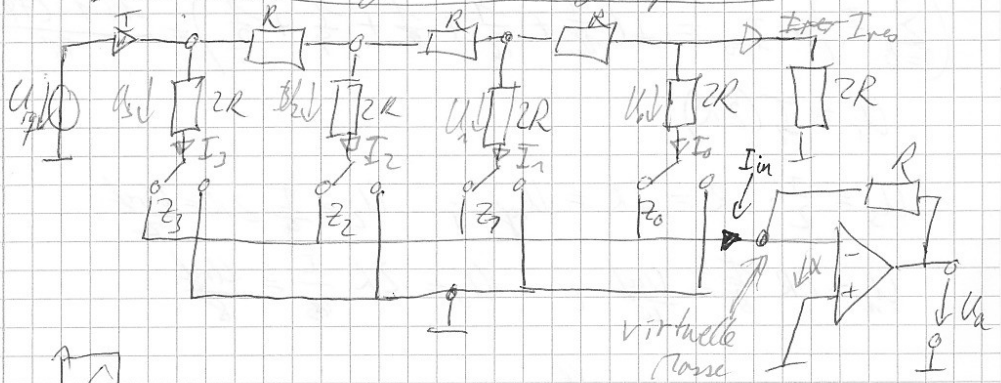
$$I_R + I_2 = 0$$

$$\frac{U_e}{R} + \frac{U_a}{Z} = 0$$

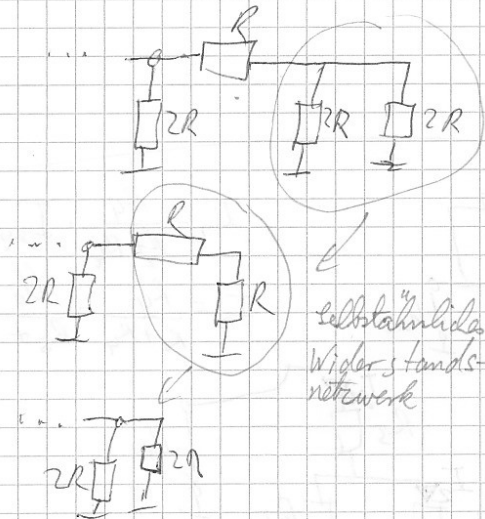
$$\frac{U_a}{U_e} = -\frac{Z}{R}; \quad Z = R \parallel Z_C = \frac{R \cdot \frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{R}{1 + j\omega RC}$$

$$H(j\omega) = -\frac{1}{1 + j\omega RC}$$

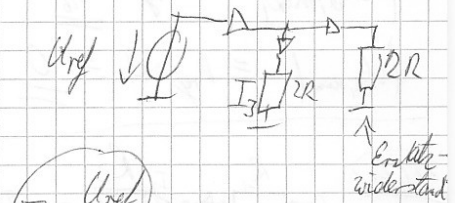
75) D/A-Umsetzung mittels Wägeverfahren



$\equiv z_3$
 $\equiv z_2$
 $\equiv z_0$



selbstähnliches
Widerstands-
netzwerk



$$I = \frac{U_{ref}}{R}$$

$$I_3 = \frac{2R}{4R} I = \frac{I}{2}$$

$$I_2 = \frac{I_3}{2} = \frac{I}{4}$$

$$I_1 = \frac{I_2}{2} = \frac{I}{8}$$

Erkenn-
widerstand

$$I_0 = \frac{I_n}{2} = \frac{I}{16} \quad ; \quad I_{res} = \frac{I}{16}$$

$$\left(\sum_{i=0}^3 I_i \right) + I_{res} = I \left(\frac{1}{16} + \frac{1}{16} + \frac{1}{8} + \frac{1}{4} + \frac{1}{2} \right) = \frac{1+1+2+4+8}{16} I = 1 \cdot I$$

$$U_i = I_i (2R)$$

$$U_3 = \frac{I}{2} \cdot 2R = IR = U_{ref} \quad ; \quad U_2 = \frac{I}{4} \cdot 2R = \frac{U_{ref}}{2}$$

$$U_1 = 2R \frac{I}{8} = \frac{U_{ref}}{4} \quad ; \quad U_0 = 2R \frac{I}{16} = \frac{U_{ref}}{8}$$

$$I_{in} + I_a \quad I_{in} + \frac{U_a}{R} = 0$$

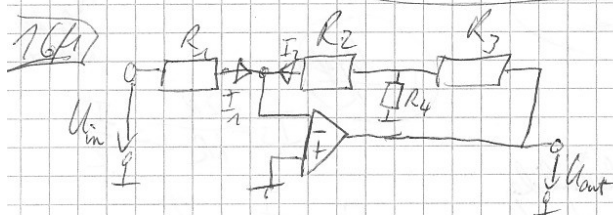
$$U_a = -R I_{in} = -R \sum_{i=0}^3 I_i z_i = -R \left(z_3 \frac{I}{2} + z_2 \frac{I}{4} + z_1 \frac{I}{8} + z_0 \frac{I}{16} \right)$$

$$= -U_{ref} \left(\frac{z_3}{2} + \frac{z_2}{4} + \frac{z_1}{8} + \frac{z_0}{16} \right) = -U_{ref} \frac{8z_3 + 4z_2 + 2z_1 + z_0}{16}$$

$$\boxed{U_a = -U_{ref} \frac{z}{16}} \quad z = 8z_3 + 4z_2 + 2z_1 + z_0$$

$$|U_{a,max}| = U_{ref} \cdot \frac{15}{16}$$

$$|U_{a,min}| = U_{ref} \cdot 0 = 0$$

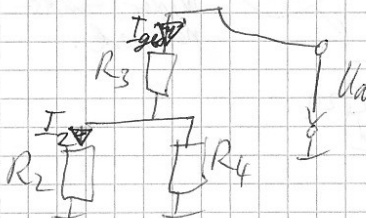


$$I_2 = \frac{R_4}{R_2 + R_4} \cdot I_{in}$$

$$I_2 = \frac{R_4}{R_2 + R_4} \cdot \frac{U_a}{R_3 + R_2 \parallel R_4}$$

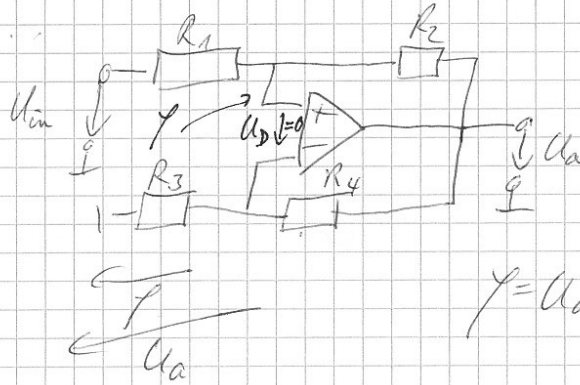
$$I_1 + I_2 = 0$$

$$\frac{U_{in}}{R_1} +$$



$$\frac{U_{in}}{R_1} + \frac{R_4}{R_2 + R_4} \cdot \frac{U_a}{R_3 + R_2 \parallel R_4} = 0 \Rightarrow U_a = \dots$$

16 (2.)



$$I = U_a \cdot \frac{R_3}{R_3 + R_4}$$

$$I_3 + I_4 = 0 ; \quad \frac{0 - I}{R_3} + \frac{U_a - I}{R_4} = 0$$

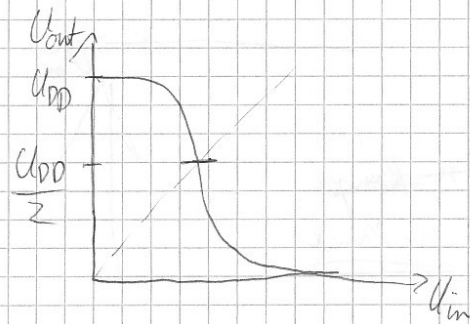
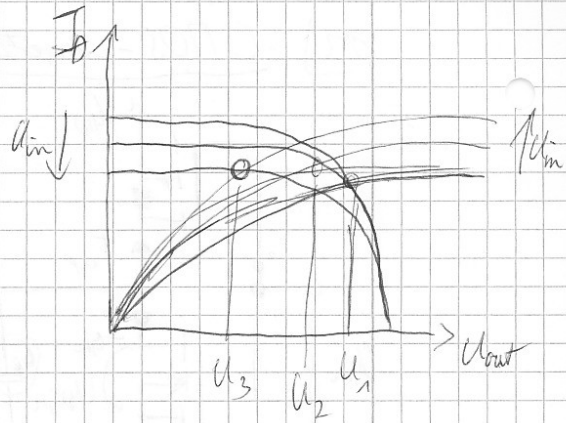
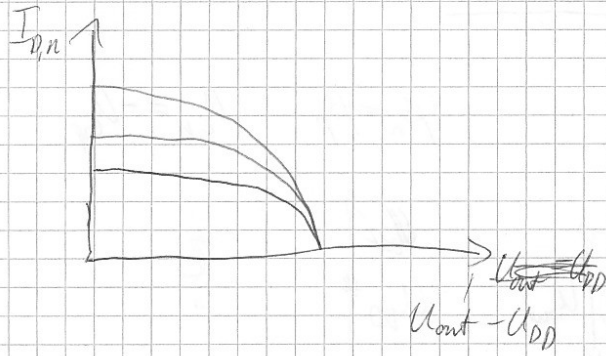
$$\frac{U_a}{R_4} = I \left(\frac{1}{R_3} + \frac{1}{R_4} \right) \Rightarrow I = \dots$$

$$\Rightarrow I = \frac{R_3 R_4}{R_3 + R_4} U_a \cdot \frac{1}{R_4}$$

$$\frac{U_{in}}{R_1} - \frac{U_a}{R_1} \frac{R_3}{R_3 + R_4} + \frac{U_a}{R_2} - \frac{U_a}{R_2} \frac{R_3}{R_3 + R_4} = 0$$

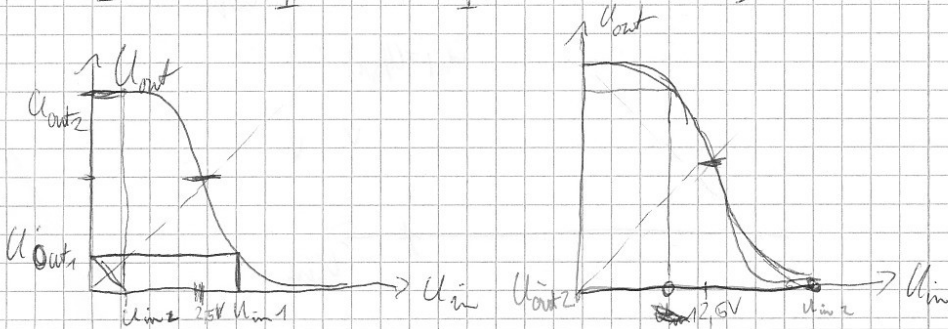
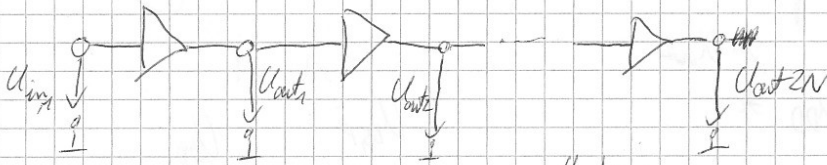
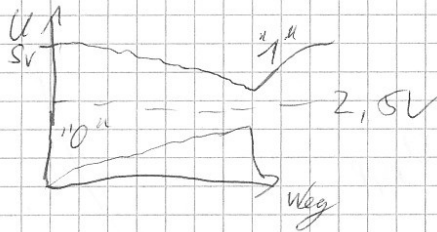
$$\frac{U_{in}}{R_1} = U_a \left[\frac{R_3}{(R_3 + R_4) R_1} + \frac{R_3}{R_2 (R_3 + R_4)} - \frac{1}{R_2} \right]$$

p-Kanal

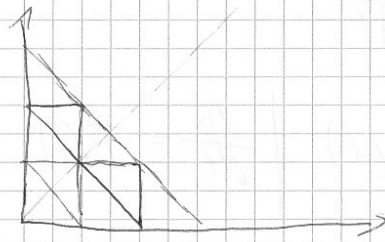


Wenn die Transistoren
selber Eingang
symmetrisch weil $\beta_n = \beta_p$

13.2 Regenerative Eigenschaften einer Inverterkette



zu 13.2



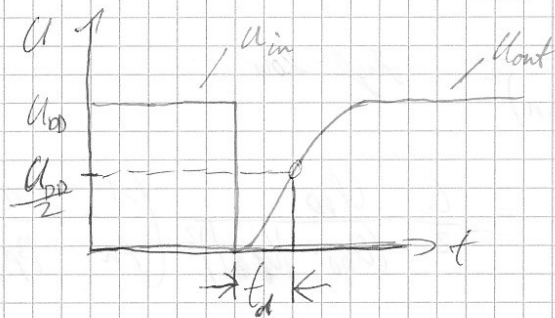
→ drehen uns im Kreis da Steigung der Kennungslinie ≤ 1 !

→ es muss gelten:

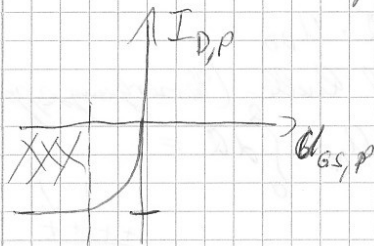
$$\left| \frac{\partial U_{out}}{\partial U_{in}} \right| > 1 \quad \left| U_{out,high} \right| \left| U_{in,high,min} \right|$$

$$\left| \frac{\partial U_{out}}{\partial U_{in}} \right| \leq 1 \quad const$$

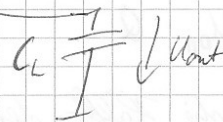
13.3) Dynamisches Verhalten



Ladestrom $i(t)$ der Kapazität kann durch einen mittleren Strom I_{ap} approximiert werden.



$$I_{ap} = \frac{\beta_p}{2} (U_{DD} - |U_{EIP}|)^2$$



$$I_{D,P} = \frac{\beta_p}{2} (U_{DD} - |U_{EIP}|)^2$$

$$C_L = \frac{Q}{U_{out}} \quad \left| \quad \frac{d}{dt} \right.$$

$$\frac{dU_{out}}{dt} = \frac{1}{C_L} i(t) \quad \left| \quad \frac{dQ}{dt} = I(t) \right.$$

$$dt = C_L \frac{dU_{out}}{i(t)}$$

$$t_d = C_L \int_0^{U_{DD}/2} \frac{dU_{out}}{i(U_{out})}$$

$$t_d = \frac{C_L}{I_{ap}} \frac{U_{DD}}{2} = \frac{C_L U_{DD}}{2} \frac{2}{\beta_P (U_{DD} - |U_{t,P}|)^2}$$

$$t_a = C_L \frac{U_{DD}}{\beta_P (U_{DD} - |U_{t,P}|)^2} \quad \text{low-high}$$

$$t_d = C_L \frac{U_{DD}}{\beta_N (U_{DD} - U_{t,N})^2} \quad \text{high-low}$$

$$b) \quad t_d = \frac{t_{d,CH} + t_{d,HL}}{2} = \frac{C_L}{2} \frac{U_{DD}}{(U_{DD} - |U_{t,N}|)^2} \left(\frac{1}{\beta_N} + \frac{1}{\beta_P} \right)$$

13.4] Dynamischer Leistungsverbrauch

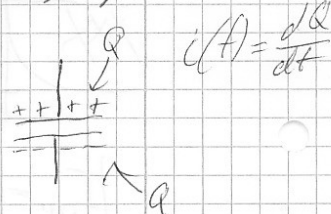
a) $0 \rightarrow 1$: Laden des Kondensators

$$W = \frac{1}{2} C_L U_{DD}^2 = \left(\frac{1}{2} \right) Q \cdot U_{DD}$$

Wieviel Energie liefert die Quell-Quelle (Versorgungsspannung)?

$$W = \int_0^Q i(t) U_{DD} dt = U_{DD} \int_0^Q dQ =$$

$$= U_{DD} \cdot Q$$



nur die Hälfte der Energie die von der Quelle kommt wird in C_L gespeichert!

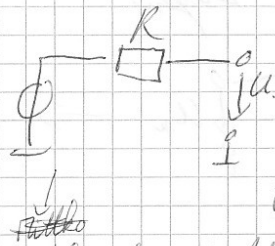
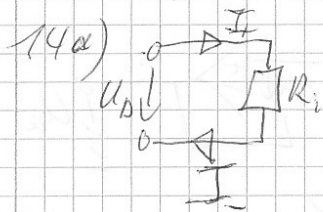
11.3 Übung

22.1.07

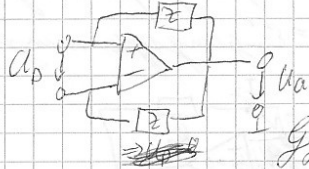
$\lambda \rightarrow 0$ gesamte Energie der Quelle geht in Wärme über! Schaltstatistik

$$c) \cdot P_{ap} = \frac{1}{T} \int_0^T i(t) U_{DD} dt = \frac{U_{DD} Q}{T} \cdot f \quad 0 \leq f \leq 1$$

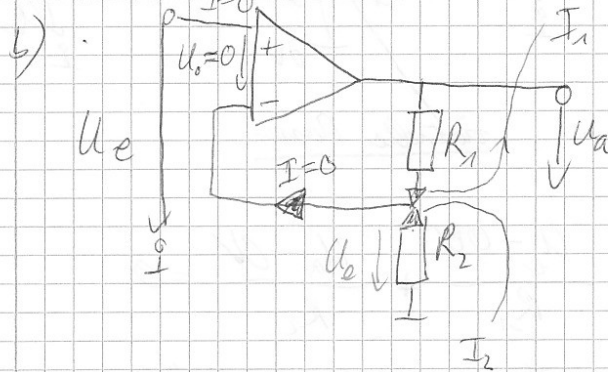
$$P_{ap} = \underset{\substack{\uparrow \\ \text{Clock}}}{f} \cdot U_{DD} Q \cdot f$$



$R_i \rightarrow \infty$
 $R_a = 0$
 $A_D \rightarrow \infty$
 idealer Op-Verstärker
 Rückkopplung - instabil \Rightarrow System schwingt



Gegenkopplung \Rightarrow $|\beta| < 1$



$+ u_a + I_2$
 $+ I_1 + I_2 = 0$

1. Schritt: Knoten gl. am Eingang vom OP

$$\frac{u_a - u_e}{R_1} + \frac{-u_e}{R_2} = 0$$

$$u_a \frac{1}{R_1} = u_e \left(\frac{1}{R_1} + \frac{1}{R_2} \right) = \frac{R_1 + R_2}{R_1 R_2} u_e$$

$$A = \frac{u_a}{u_e} = \frac{R_1 + R_2}{R_2} = 1 + \frac{R_1}{R_2}$$

2. Schritt

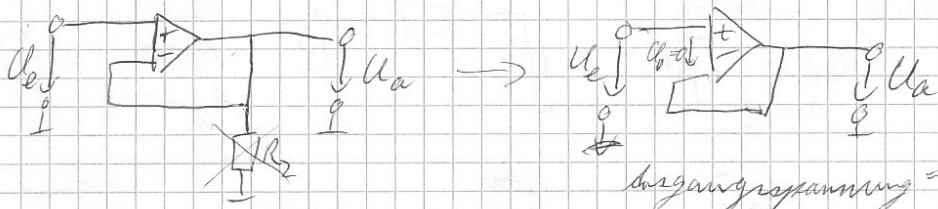
Einsetzen der Ströme durch u_a, u_e und Impedanzen.

$$u_e = \frac{R_2}{R_1 + R_2} u_a \quad \text{Spannungsteiler}$$

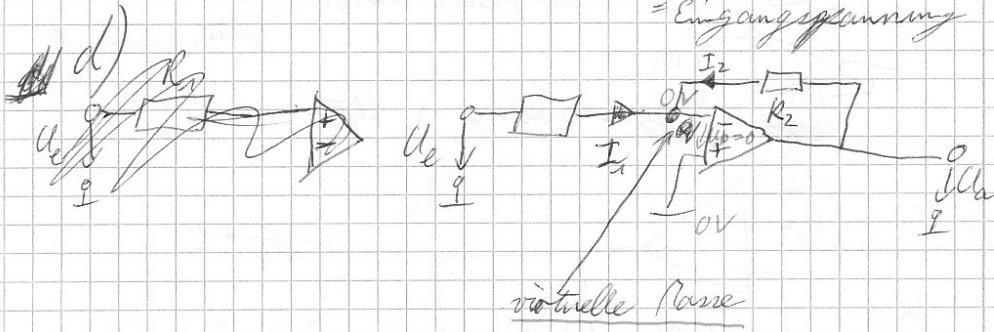
~~OP~~

c) $R_1 \rightarrow 0$
 $\lim_{R_1 \rightarrow 0} A = 1 \Rightarrow \boxed{u_a = u_e}$ Spannungsföher

Entkopplung von Stufen



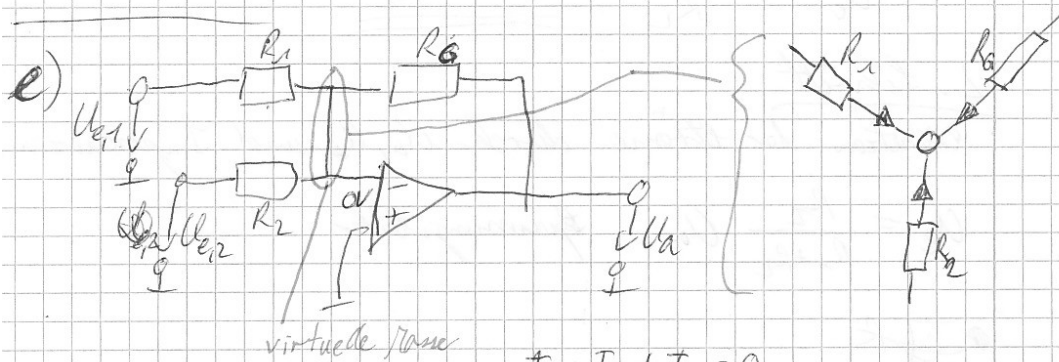
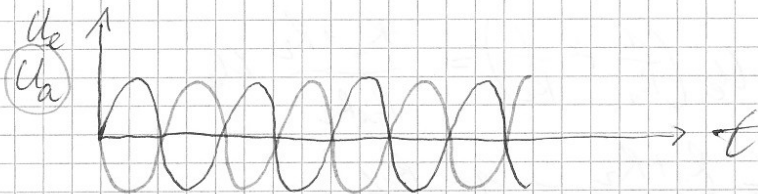
Ausgangsspannung =
Eingangsspannung



virtuelle Masse

$$\Rightarrow I_1 + I_2 = 0; \quad \frac{U_e - 0V}{R_1} + \frac{U_a - 0V}{R_2} = 0$$

$$\Rightarrow \frac{U_a}{U_e} = - \frac{R_2}{R_1} \quad \text{Invertierender Verstärker}$$



virtuelle Masse

$$I_1 + I_2 + I_3 = 0$$

$$\frac{U_{e1} - 0V}{R_1} + \frac{U_{e2} - 0V}{R_2} + \frac{U_a}{R_3} = 0$$

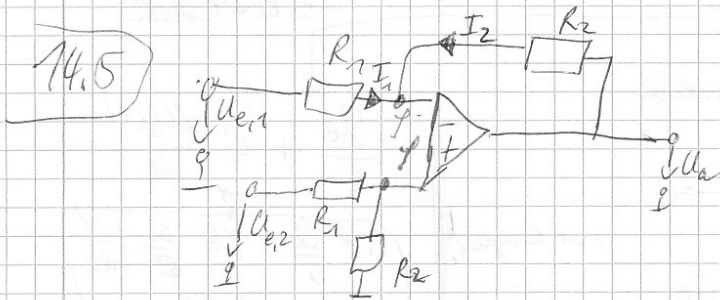
T13 - Übung

28.1.07

$$U_a = -R_G \left(\frac{U_{e1}}{R_1} + \frac{U_{e2}}{R_2} \right)$$

$$U_a = \left(\frac{R_G}{R_1} \cdot U_{e1} + \frac{R_G}{R_2} \cdot U_{e2} \right)$$

$(z = -(\alpha x_1 + \beta x_2))$
 Invertierende Addierer



$$f = U_{e2} \cdot \frac{R_2}{R_1 + R_2}$$

$$I_1 + I_2 = 0 \quad \frac{U_{e1}}{R_1} + \frac{U_a - f}{R_2} = 0$$

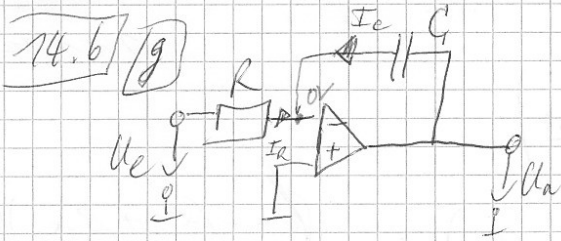
$$\frac{U_{e1} - U_{e2} \cdot \frac{R_2}{R_1 + R_2}}{R_2} + \frac{U_a}{R_2} - \frac{U_{e2} R_2}{(R_1 + R_2) \cdot R_2} = 0$$

$$-\frac{U_a}{R_2} = \frac{U_{e1}}{R_1} - \frac{U_{e2}}{R_1 + R_2} \left(\frac{R_2}{R_1} + 1 \right)$$

$$U_a = -\frac{R_2}{R_1} \cdot U_{e1} + U_{e2} \frac{R_2}{R_1 + R_2} \cdot \frac{R_2 + R_1}{R_1}$$

$$U_a = \frac{R_2}{R_1} \cdot (U_{e2} - U_{e1}) \quad z = \alpha(x_1 - x_2)$$

Nicht invertierende Subtraktion



$$\frac{U_a}{R} + I_C = 0$$

$$I_R + I_C = 0$$

zeitbereich

Frequenzbereich

$$\frac{U_e}{R} + \frac{U_a}{\frac{1}{j\omega C}} = 0$$

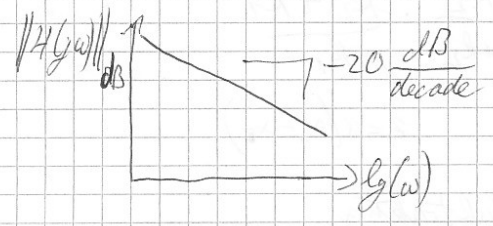
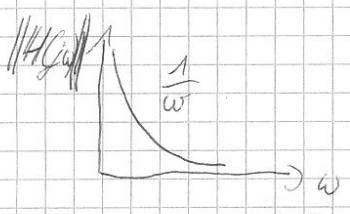
j ist komplex!

$$-U_a j\omega C = \frac{U_e}{R}$$

$$\Rightarrow H(j\omega) = \frac{U_a}{U_e} = -\frac{1}{j\omega RC}$$

$$H(j\omega) = \frac{j}{\omega RC}$$

$$\|H(j\omega)\| = \frac{1}{\omega RC}$$



$$\frac{U_e}{R} + C \frac{dU_a(t)}{dt} = 0$$

$$C = \frac{Q}{u}, U = \frac{Q}{C} \left| \frac{d}{dt} \right.$$

$$I_C(t) = C \frac{dU_e}{dt}$$

$$\frac{dU_a}{dt} = -\frac{1}{RC} U_e(t)$$

$$U_a(t) - U_a(t=0) = -\frac{1}{RC} \int_0^t U_e(t) dt$$

$$\int f(x) dx \rightarrow \frac{F(\omega)}{j\omega}$$